# ANALYSIS OF CURVED BEAMS 

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#### Abstract

Analysis of curved beam is a vital part of structural analysis as curved beams have found many applications in civil, mechanical and aerospace engineering. This Dissertation developed a computer aided analysis of a "curved beam-element" using Stiffness matrix method. A Microsoft Excel Spreadsheet program was developed and used to analyze the curved beam element. The main assumption is that the curve is made up of finite straight lines therefore stiffness matrix method of analysis is suitable to analyze the curved beam. Abaqus software was used to validate the results obtained from the Excel spreadsheet and the \% difference were calculated. The \% difference obtained were within acceptable limit so MS Excel program developed can be used to analyze beams. Almost everyone's business or personal computer has Excel installed, which makes it a trustworthy way to transfer information and easy access. For every computer literate that can use the MS Excel Spreadsheet even if you do not know how to use Abaqus, Ansys, FEM or other engineering software which are not always available on all computers, can use the MS Excel spreadsheet to analyze curved beams. The straight beam approximation method is a reliable method to calculate curved beam elements of different section.


Keywords: curved, beam, analysis, Ms excel, stiffness matrix.

## 1. INTRODUCTION

Curved beams are used in civil, mechanical and aerospace engineering. Beam whose axis is not straight and is curved in the elevation is said to be a curved beam. If the applied loads are along the $y$ direction and the span of the beam is along the $x$ direction, the axis of the beam should have a curvature in the $x y$ plane. On the other hand, if the member is curved on the xz plane with the loading still along the y direction, then it is not a curved beam, as this loading will cause a bending as well as twisting of the section. Thus, a curved beam does not have a curvature in the plan. Arches are examples of curved beams.

Curved beams could be analyzed with different softwares like Ansy, Abaqus, FEM, etc but these softwares are not available on all computers. This dissertation focuses on producing a MS Excel program that could be used to analyze curved beams of different sections and materials. The spreadsheet produced could be used on all computer systems and phones that support Microsoft office files.

## 2. THE FINITE ELEMENT METHOD

The "finite element method" in structural analysis is a method in which an actual continuous structure is replaced by a mathematical model made up from structural elements of finite size having known material and geometrical properties. The complete structure is then analyzed as an assemblage of these discrete elements, where every such element is treated as a continuous structural member. It is a requirement in this method of structural analysis that the displacements be compatible and the internal forces be in balance at points on the complete structure shared by two or more elements [13]. Such points are called "joints" or "nodes."

The material and geometric properties of each element relate the displacements to the applied generalized forces at each point of the structural element. Thus these properties are called the "force displacement properties" [2] and are related to and depend upon three properties: the stress-strain properties of the material from which the structural element is made, the geometry and sectional properties of the element and the displacement or forces imposed at the boundaries of the structural element.

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These force-displacement relationships are usually found either by determining displacements resulting from a known set of forces in equilibrium or determining a set of forces in equilibrium that are required to produce a prescribed configuration of the structural element. These two methods of finding the displacement-force or force-displacement relationships result in two corresponding matrices involving the material and geometric properties of the structural element. The former method results in what is called the "flexibility matrix" while the result of the latter method is the "stiffness matrix the two matrices relate forces and displacements in the following manner:

$$
\begin{aligned}
& \{\mathrm{v}\}=[\mathrm{a}](\mathrm{f}) \\
& (\mathrm{F})=[\mathrm{k}]\{\mathrm{v}\}
\end{aligned}
$$

Where $\{\mathrm{v}\}=$ a generalized displacement vector of n components.
$\{\mathrm{F}\}=$ a generalized force vector of n components.
[a] = an nth order square matrix containing the flexibility Coefficients.
$[\mathrm{k}]=$ an nth order square matrix containing the stiffness Coefficients.

## 3. STIFFNESS METHOD

As one of the methods of structural analysis, the direct stiffness method, also known as the matrix stiffness method, is particularly suited for computer-automated analysis of complex structures including the statically indeterminate type. It is a matrix method that makes use of the members' stiffness relations for computing member forces and displacements in structures. The direct stiffness method is the most common implementation of the finite element method (FEM). In applying the method, the system must be modeled as a set of simpler, idealized elements interconnected at the nodes. The material stiffness properties of these elements are then, through matrix mathematics, compiled into a single matrix equation which governs the behaviour of the entire idealized structure. The structure's unknown displacements and forces can then be determined by solving this equation. The direct stiffness method forms the basis for most commercial and free source finite element software.

The direct stiffness method originated in the field of aerospace. Researchers looked at various approaches for analysis of complex airplane frames. These included elasticity theory, energy principles in structural mechanics, flexibility method and matrix stiffness method. It was through analysis of these methods that the direct stiffness method emerged as an efficient method ideally suited for computer implementation.

## 4. SIMPLE USE OF THE PRE-WRITTEN PROGRAM

## The straight beam approximations (stiffness method)

$>\quad$ Insert the individual properties of each beam element on the member properties table (Table 3.1: Input table).
$>\quad$ Insert the nodal force on the Nodes Table (table 3.2 : Input table for external forces on the Nodes)
$>\quad$ To obtain the displacements on the nodes of the structure, we use the formula:
> $\quad \mathrm{D}=\mathrm{K}^{-1} * \mathrm{~F}$
$>\quad$ Where:
> $\mathrm{D}=$ Displacement
> $\quad \mathrm{K}=$ Global Stiffness Matrix
$>\quad \mathrm{K}^{-1}=$ Inverse of the global stiffness matrix
> $\mathrm{F}=$ Applied forces

## 5. EXTRACTED EXAMPLES FROM MY DISSERTATION

Question 1: Find the displacements, reactions and final forces of the frame in Fig. Q1 below.

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Fig.Q1
Table Q1.1: Properties of all Members in the Frame

| MEMBER PROPERTIES |  |  |  |  |  |  | $\mathbf{A}\left(\mathbf{m}^{\mathbf{2}}\right)$ | $\mathbf{I}\left(\mathbf{m}^{\mathbf{4}}\right)$ | $\mathbf{E}\left(\mathbf{K N} / \mathbf{m}^{\mathbf{2}}\right)$ | $(\boldsymbol{\theta})$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| MEMBER | $\mathbf{L}(\mathbf{m})$ | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 90 |  |  |  |  |  |
| AC | 3.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 67.5 |  |  |  |  |  |
| CD | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 45 |  |  |  |  |  |
| DE | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 22.5 |  |  |  |  |  |
| EF | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 0 |  |  |  |  |  |
| FG | 2.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 337.5 |  |  |  |  |  |
| GH | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 315 |  |  |  |  |  |
| HI | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 292.5 |  |  |  |  |  |
| IJ | 1.000 | 0.053 | 0.000233 | $3.0 \mathrm{E}+04$ | 270 |  |  |  |  |  |
| BJ | 3.000 |  |  |  |  |  |  |  |  |  |

Table Q1.2: Forces on each Node of the frame

| NODES (kN) |  |  |  |
| :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{AX}}$ | 0 | $\mathrm{P}_{\text {FX }}$ | 0 |
| $\mathrm{P}_{\text {AY }}$ | 0 | $\mathrm{P}_{\mathrm{FY}}$ | 5 |
| $\mathrm{M}_{\mathrm{A}}$ | 0 | $\mathrm{M}_{\mathrm{F}}$ | 0 |
| $\mathrm{P}_{\text {BX }}$ | 0 | $\mathrm{P}_{\text {GX }}$ | 0 |
| $\mathrm{P}_{\text {BY }}$ | 0 | $\mathrm{P}_{\text {GY }}$ | 5 |
| $\mathrm{M}_{\mathrm{B}}$ | 0 | $\mathrm{M}_{\mathrm{G}}$ | 0 |
| $\mathrm{P}_{\mathrm{CX}}$ | 10 | $\mathrm{P}_{\mathrm{HX}}$ | 0 |
| $\mathrm{P}_{\mathrm{CY}}$ | 0 | $\mathrm{P}_{\mathrm{HY}}$ | 0 |
| $\mathrm{M}_{\mathrm{C}}$ | 0 | $\mathrm{M}_{\mathrm{H}}$ | 0 |
| $\mathrm{P}_{\mathbf{D X}}$ | 0 | $\mathrm{P}_{\text {IX }}$ | 0 |
| $\mathrm{P}_{\text {DY }}$ | 0 | $\mathrm{P}_{\text {IY }}$ | 0 |
| $\mathrm{M}_{\mathrm{D}}$ | 0 | $\mathrm{M}_{\mathrm{I}}$ | 0 |
| $\mathrm{P}_{\text {EX }}$ | 0 | $\mathrm{P}_{\mathrm{JX}}$ | 0 |
| $\mathrm{P}_{\text {EY }}$ | 0 | $\mathrm{P}_{\mathrm{JY}}$ | 0 |
| $\mathrm{M}_{\mathrm{E}}$ | 0 | $\mathrm{M}_{\mathrm{J}}$ | 0 |



Fig.Q1.1: Loading and Boundary conditions


Fig.Q1.10: SS1 plot


Fig.Q1.11: Bending Moment Diagram (Full Path)

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The results obtained from the MS Excel Spreadsheet and Abaqus for Question 1 are displayed in table Q1.3, Q1.4 and Q1.5 below.

Table Q1.3: Member Displacement Result

|  | MS EXCEL | ABAQUS | \% DIFF |
| :---: | :---: | :---: | :---: |
| $\Delta_{\text {AX }}$ | 0 | 5.48E-33 |  |
| $\Delta_{\text {AY }}$ | 0 | $3.42 \mathrm{E}-33$ |  |
| $\boldsymbol{\theta}_{\text {A }}$ | 0 | $1.08 \mathrm{E}+04$ |  |
| $\Delta_{\text {CX }}$ | 4.777 | 4.69817 | 1.646081 |
| $\Delta_{\text {CY }}$ | 0.012 | $1.27 \mathrm{E}-02$ | 2.592302 |
| $\boldsymbol{\theta}_{\text {C }}$ | -1.179 | $1.26 \mathrm{E}+00$ | 6.452381 |
| $\Delta_{\text {CX }}$ | 4.777 | 4.64817 | 2.692807 |
| $\Delta_{\text {CY }}$ | 0.012 | $1.27 \mathrm{E}-02$ | 2.592302 |
| $\boldsymbol{\theta}_{\text {C }}$ | -1.179 | $-1.26 \mathrm{E}+00$ | 6.89743 |
| $\Delta_{\text {DX }}$ | 5.191 | 5.048 | 2.752894 |
| $\Delta_{\text {DY }}$ | -0.155 | -0.1671 | 7.73694 |
| $\boldsymbol{\theta}_{\text {D }}$ | 0.211 | 0.18 | 14.73235 |
| $\Delta_{\text {DX }}$ | 5.191 | 5.08 | 2.136431 |
| $\Delta_{\text {DY }}$ | -0.155 | -0.1494 | -3.81526 |
| $\boldsymbol{\theta}_{\text {D }}$ | 0.211 | 0.22815 | 7.473154 |
| $\Delta_{\text {EX }}$ | 4.717 | 5.0128 | 5.896904 |
| $\Delta_{\text {EY }}$ | 0.322 | 0.299 | 7.229289 |
| $\boldsymbol{\theta}_{\text {E }}$ | 1.012 | 0.98159 | 3.014524 |
| $\Delta_{\text {EX }}$ | 4.717 | 5.043 | 6.46044 |
| $\Delta_{\text {EY }}$ | 0.322 | 0.296 | 8.160099 |
| $\boldsymbol{\theta}_{\text {E }}$ | 1.012 | 0.98132 | 3.041201 |
| $\Delta_{\text {FX }}$ | 4.305 | 4.60066 | 6.417775 |
| $\Delta_{\mathrm{FY}}$ | 1.32 | $1.20 \mathrm{E}+00$ | 9.278569 |
| $\boldsymbol{\theta}_{\text {F }}$ | 0.995 | 1.015 | 1.970443 |
| $\Delta_{\text {FX }}$ | 4.305 | 4.460066 | 3.467796 |
| $\Delta_{\mathrm{FY}}$ | 1.32 | $1.27 \mathrm{E}+00$ | 3.637466 |
| $\boldsymbol{\theta}_{\text {F }}$ | 0.995 | 1.015 | 1.970443 |
| $\Delta_{\mathrm{GX}}$ | 4.305 | 4.59496 | 6.319097 |
| $\Delta_{\text {GY }}$ | 2.07 | $1.89 \mathrm{E}+00$ | 8.730734 |
| $\boldsymbol{\theta}_{\mathrm{G}}$ | -0.395 | -0.37824 | 4.48393 |
| $\Delta_{\mathbf{G X}}$ | 4.305 | 4.59496 | 6.319097 |
| $\Delta_{\text {GY }}$ | 2.07 | $1.89 \mathrm{E}+00$ | 8.730734 |
| $\boldsymbol{\theta}_{\text {G }}$ | -0.395 | -0.37824 | 4.48393 |
| $\Delta_{\text {HX }}$ | 4.009 | 3.89496 | 2.837329 |
| $\Delta_{\mathrm{HY}}$ | 1.354 | 1.267 | 6.439226 |
| $\boldsymbol{\theta}_{\mathrm{H}}$ | -1.072 | -0.99722 | 7.47879 |
| $\Delta_{\text {HX }}$ | 4.009 | 4.18 | 4.098086 |
| $\Delta_{\mathrm{HY}}$ | 1.354 | 1.358 | 0.279823 |
| $\boldsymbol{\theta}_{\mathrm{H}}$ | -1.072 | -1.1599 | 8.21982 |
| $\Delta_{\text {IX }}$ | 3.147 | 3.143 | 0.139798 |
| $\Delta_{\text {IV }}$ | 0.491 | 0.485 | 1.262215 |
| $\boldsymbol{\theta}_{\text {I }}$ | -1.298 | -1.395 | 7.47304 |
| $\Delta_{\text {IX }}$ | 3.147 | 2.92 | 7.225011 |
| $\Delta_{\text {IV }}$ | 0.491 | 0.502 | 2.151394 |
| $\boldsymbol{\theta}_{\text {I }}$ | -1.298 | -1.1955 | 8.57382 |
| $\Delta_{\text {JX }}$ | 1.982 | 2.152196 | 7.912662 |

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| $\boldsymbol{\Delta}_{\mathbf{J Y}}$ | 0.006 | $5.91 \mathrm{E}-03$ | 9.04 |
| :--- | :--- | :--- | :--- |
| $\boldsymbol{\theta}_{\mathbf{J}}$ | -1.181 | -1.20986045 | 2.42638 |
| $\boldsymbol{\Delta}_{\mathbf{B X}}$ | 0 | $4.52 \mathrm{E}-33$ |  |
| $\boldsymbol{\Delta}_{\mathbf{B Y}}$ | 0 | $6.58 \mathrm{E}-33$ |  |
| $\boldsymbol{\theta}_{\mathbf{B}}$ | 0 | 0.000056 |  |
| $\boldsymbol{\Delta}_{\mathbf{J X}}$ | 1.982 | 2.152196 | 7.912662 |
| $\boldsymbol{\Delta}_{\mathbf{J Y}}$ | 0.006 | $5.92 \mathrm{E}-03$ | 8.861538 |
| $\boldsymbol{\theta}_{\mathbf{J}}$ | -1.181 | -1.20913 | 2.36454 |

Table Q1.4: Reactions on the Nodes of the Frame

|  | MS EXCEL | ABAQUS | \% DIFF |
| :---: | :---: | :---: | :---: |
| $\mathbf{P}_{\text {ACX }}$ | -9.3473 | -10.0048 | 7.03412 |
| $\mathbf{P}_{\text {ACY }}$ | -6.5764 | -6.6157 | 0.59759 |
| $\mathbf{M}_{\text {AC }}$ | 16.76733 | 16.456 | 1.85659 |
| $\mathbf{P}_{\text {CaX }}$ | 9.347299 | 9.256 | 0.976753 |
| $\mathbf{P}_{\text {CAY }}$ | 6.576397 | 6.496 | 1.222553 |
| $\mathbf{M C A}^{\text {Ca }}$ | 11.27457 | 10.946 | 2.914516 |
| $\mathbf{P}_{\text {CDX }}$ | 0.652701 | 0.6558 | 0.472705 |
| $\mathbf{P}_{\text {CDY }}$ | -6.5764 | -6.998 | 6.4108 |
| $\mathbf{M}_{\text {CD }}$ | -11.2746 | -11.44 | 1.46701 |
| $\mathbf{P}_{\text {DCX }}$ | -0.6527 | -0.64511 | 1.17654 |
| $\mathbf{P}_{\text {DCY }}$ | 6.576397 | 7.01585 | 6.263674 |
| $\mathbf{M}_{\text {DC }}$ | 8.154872 | 7.887 | 3.285141 |
| $\mathbf{P}_{\text {DEX }}$ | 0.652701 | 0.6258 | 4.121342 |
| $\mathbf{P}_{\text {DEY }}$ | -6.5764 | -6.995 | 6.36518 |
| $\mathrm{M}_{\text {DE }}$ | -8.15487 | -7.9582 | 2.47166 |
| $\mathbf{P}_{\text {EdX }}$ | -0.6527 | -0.696 | 6.63398 |
| $\mathbf{P}_{\text {EDY }}$ | 6.576397 | 7.0246 | 6.380434 |
| $\mathbf{M E D}^{\text {E }}$ | 3.043128 | 2.859 | 6.049752 |
| $\mathbf{P}_{\text {EfX }}$ | 0.652701 | 0.696 | 6.221264 |
| $\mathbf{P}_{\text {EFY }}$ | -6.5764 | -6.992 | 6.36518 |
| $\mathbf{M E F}^{\text {EF }}$ | -3.04313 | -2.852 | 6.70056 |
| $\mathbf{P}_{\text {FEX }}$ | -0.6527 | -0.6496 | 0.47722 |
| $\mathbf{P}_{\text {FEY }}$ | 6.576397 | 6.47857 | 1.487592 |
| $\mathbf{M}_{\text {FE }}$ | -3.28245 | -3.456 | 5.28881 |
| $\mathbf{P}_{\text {FGX }}$ | 0.652701 | 0.5986 | 8.288647 |
| $\mathbf{P}_{\text {FGY }}$ | -1.5764 | -1.617 | 2.57549 |
| $\mathbf{M F G}_{\text {FG }}$ | 3.282449 | 3.198 | 2.571289 |
| $\mathbf{P}_{\text {GFX }}$ | -0.6527 | -0.6791 | 4.04474 |
| $\mathbf{P}_{\text {GFY }}$ | 1.576397 | 1.61686 | 2.502381 |
| $\mathbf{M}_{\text {GF }}$ | -6.43524 | -5.9576 | 8.01665 |
| $\mathbf{P}_{\text {GHX }}$ | 0.652701 | 0.646 | 1.026505 |
| $\mathbf{P}_{\text {GHY }}$ | 3.423603 | 3.591 | 4.661654 |
| $\mathbf{M}_{\text {GH }}$ | 6.435242 | 6.572 | 2.081558 |
| $\mathbf{P}_{\text {HGX }}$ | -0.6527 | -0.644 | 1.35093 |
| $\mathbf{P}_{\text {HGY }}$ | -3.4236 | -3.582 | 4.62671 |
| $\mathbf{M H G}_{\text {HG }}$ | -3.02247 | -2.96 | 2.11149 |
| $\mathbf{P}_{\text {HIX }}$ | 0.652701 | 0.67 | 2.58209 |
| $\mathbf{P}_{\text {HIY }}$ | 3.423603 | 3.72 | 7.967742 |
| $\mathrm{M}_{\mathrm{HI}}$ | 3.022468 | 2.81 | 7.030604 |
| $\mathbf{P}_{\text {IHX }}$ | -0.6527 | -0.68 | 4.18263 |

Page | 119

International Journal of Civil and Structural Engineering Research ISSN 2348-7607 (Online) Vol. 6, Issue 1, pp: (114-123), Month: April - September 2018, Available at: www.researchpublish.com

| $\mathbf{P}_{\mathbf{I H Y}}$ | -3.4236 | -3.49 | 1.93948 |
| :--- | :--- | :--- | :--- |
| $\mathbf{M}_{\mathbf{I H}}$ | -0.14009 | -0.1469 | 4.85368 |
| $\mathbf{P}_{\text {IJX }}$ | 0.652701 | 0.6397 | 1.991727 |
| $\mathbf{P}_{\text {IJY }}$ | 3.423603 | 3.554 | 3.669105 |
| $\mathbf{M}_{\mathbf{I J}}$ | 0.140086 | 0.1385 | 1.142041 |
| $\mathbf{P}_{\text {JIX }}$ | -0.6527 | -0.71 | 8.77892 |
| $\mathbf{P}_{\mathbf{J I Y}}$ | -3.4236 | -3.387 | 1.0806 |
| $\mathbf{M}_{\mathbf{I I}}$ | 1.773087 | 1.799 | 1.439689 |
| $\mathbf{P}_{\text {BJX }}$ | -11.6613 | -12.17 | 4.36319 |
| $\mathbf{P}_{\mathbf{B J Y}}$ | -3.4236 | -3.368 | 1.65083 |
| $\mathbf{M}_{\text {BJ }}$ | -14.7397 | -15.02 | 1.90167 |
| $\mathbf{P}_{\mathbf{J B X}}$ | 11.66125 | 12.07 | 3.38691 |
| $\mathbf{P}_{\mathbf{J B Y}}$ | 3.423603 | 3.368 | 1.624021 |
| $\mathbf{M}_{\mathbf{J B}}$ | -20.244 | -19.702 | 2.75099 |

Table Q1.5: Final Member Forces of the Frame

|  | MS EXCEL | ABAQUS | \% DIFF |
| :---: | :---: | :---: | :---: |
| $\mathbf{P}_{\text {ACX }}$ | -6.576 | -6.59 | 0.2068 |
| $\mathbf{P}_{\text {ACY }}$ | 9.347 | 8.918 | 4.59277 |
| $\mathbf{M}_{\text {AC }}$ | 16.77 |  |  |
| $\mathbf{P}_{\text {Cax }}$ | 6.576 | 6.59 | 0.206373 |
| $\mathbf{P}_{\text {CAY }}$ | -9.347 | -8.918 | 4.81386 |
| $\mathbf{M}_{\text {CA }}$ | 11.27 |  |  |
| $\mathbf{P}_{\text {CDX }}$ | -5.826 | -6.087 | 4.47992 |
| $\mathbf{P}_{\text {CDY }}$ | -3.12 | -2.95789 | 5.47045 |
| $\mathbf{M}_{\text {CD }}$ | -11.27 |  |  |
| $\mathbf{P}_{\text {DCX }}$ | 5.826 | 6.0287 | 3.362251 |
| $\mathbf{P}_{\text {DCY }}$ | 3.12 | 3.0789 | 1.307818 |
| $\mathbf{M}_{\text {DC }}$ | 8.155 |  |  |
| $\mathbf{P}_{\text {DEX }}$ | -4.189 | -3.9814 | 5.20671 |
| $\mathbf{P}_{\text {DEY }}$ | -5.112 | -5.245 | 2.60774 |
| $\mathbf{M}_{\text {DE }}$ | -8.155 |  |  |
| $\mathbf{P}_{\text {EdX }}$ | 4.189 | 4.278 | 2.087424 |
| $\mathrm{P}_{\text {EdY }}$ | 5.112 | 4.945 | 3.261146 |
| $\mathbf{M}_{\text {ED }}$ | 3.043 |  |  |
| $\mathbf{P}_{\text {EfX }}$ | -1.914 | -1.98 | 3.46449 |
| $\mathbf{P}_{\text {EFY }}$ | -6.326 | -6.48 | 2.44088 |
| $\mathbf{M}_{\text {EF }}$ | -3.043 |  |  |
| $\mathbf{P}_{\text {FEX }}$ | 1.914 | 2.0287 | 5.668655 |
| $\mathbf{P}_{\text {FEY }}$ | 6.326 | 6.178 | 2.333375 |
| $\mathbf{M}_{\text {FE }}$ | -3.282 |  |  |
| $\mathbf{P}_{\text {FGX }}$ | 0.653 | 0.641675 | 1.689137 |
| $\mathbf{P}_{\text {FGY }}$ | -1.576 | -1.54849 | 1.8024 |
| $\mathbf{M}_{\text {FG }}$ | 3.282 |  |  |
| $\mathbf{P}_{\text {GFX }}$ | -0.653 | -0.621675 | 4.99055 |
| $\mathbf{P}_{\text {GFY }}$ | 1.576 | 1.4849 | 5.804364 |
| $\mathbf{M}_{\text {GF }}$ | -6.435 |  |  |
| $\mathbf{P}_{\text {GHX }}$ | -0.707 | -0.7568 | 7.02871 |
| $\mathbf{P}_{\text {GHY }}$ | 3.413 | 3.68 | 7.26087 |
| $\mathbf{M}_{\text {GH }}$ | 6.435 |  |  |

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| $\mathbf{P}_{\text {HGX }}$ | 0.707 | 0.71568 | 1.19886 |
| :---: | :---: | :---: | :---: |
| $\mathrm{P}_{\mathrm{HGY}}$ | -3.413 | -3.368 | 1.33017 |
| $\mathrm{M}_{\text {HG }}$ | -3.022 |  |  |
| $\mathbf{P}_{\text {HIX }}$ | -1.959 | -1.84 | 6.4837 |
| $\mathbf{P}_{\text {HIY }}$ | 2.882 | 2.7921 | 3.132806 |
| $\mathrm{M}_{\mathrm{HI}}$ | 3.022 |  |  |
| $\mathrm{P}_{\text {IHX }}$ | 1.959 | 2.0754 | 5.594102 |
| $\mathrm{P}_{\text {IHY }}$ | -2.882 | -3.021 | -4.80849 |
| $\mathbf{M}_{\text {IH }}$ | -0.14 |  |  |
| $\mathbf{P}_{\text {IJX }}$ | -2.913 | -3.1047 | 6.57353 |
| $\mathbf{P}_{\text {IJY }}$ | 1.913 | 1.891 | 1.16036 |
| $\mathrm{M}_{\mathrm{IJ}}$ | 0.14 |  |  |
| $\mathbf{P}_{\text {JIX }}$ | 2.913 | 3.012 | 3.280212 |
| $\mathbf{P}_{\text {JIY }}$ | -1.913 | -2.0172 | 5.43592 |
| $\mathrm{M}_{\text {JI }}$ | 1.773 |  |  |
| $\mathbf{P}_{\text {BJX }}$ | 3.424 | 3.25 | 5.070686 |
| $\mathbf{P}_{\text {BJY }}$ | -11.66 | -11.024 | 5.78012 |
| $\mathbf{M}_{\text {BJ }}$ | -14.74 |  |  |
| $\mathbf{P}_{\text {JBX }}$ | -3.424 | -3.34 | 2.50299 |
| $\mathbf{P}_{\text {JBY }}$ | 11.66 | 11.131 | 4.546702 |
| $\mathbf{M}_{\text {JB }}$ | -20.24 |  |  |

The percentage difference between the results obtained from the abaqus and the MS Excel calculation sheet is within acceptable limit. Therefore, this proves that the MS Excel calculation sheet is a good one for calculating curved beams.

To further validate the results from the MS Excel program we solved a problem solved as an example in page 412 of STRUCTURAL ANALYSIS USING CLASSICAL AND MATRIX METHOD, written by JAMES K. NELSON AND JACK C. MCCORMAC THIRD EDITION and the results are compared below.

Question 5: Find the final forces of the frame in Fig. Q5 below.


Fig.Q5
The results obtained from the MS Excel and that of the textbook are shown below in table Q5.2 together with the \% difference.

Table Q 5.1: Properties of all Members in the Frame

| MEMBER PROPERTIES |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| MEMBER | $\mathrm{L}(\mathrm{ft})$ | $\mathrm{A}\left(\mathrm{m}^{2}\right)$ | $\mathrm{I}\left(\mathrm{m}^{4}\right)$ | $\mathrm{E}\left(\mathrm{KN} / \mathrm{m}^{2}\right)$ | $(\theta)$ |  |
| AC | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 90 |  |
| CD | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 90 |  |

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| DE | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 90 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| EF | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 0 |
| FG | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 0 |
| GH | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 0 |
| HI | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 270 |
| IJ | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 270 |
| BJ | 10 | 0.053 | 0.0002332 | $3.0 \mathrm{E}+04$ | 270 |

Table Q5.2: Final Member Forces of the Frame

|  | Textbook <br> (kips), (k-ft) | MS Excel <br> (kips), (k-ft) | $\%$ Diff |
| :--- | :--- | :--- | :--- |
| $\mathrm{P}_{\text {ACX }}$ | -13.93 | -13.53 | 2.95639 |
| $\mathrm{P}_{\text {ACY }}$ | 2.67 | 2.215 | 17.0412 |
| $\mathrm{M}_{\text {AC }}$ | 26.7 | 19.1 | 28.46442 |
| $\mathrm{P}_{\mathrm{CAX}}$ | 13.93 | 13.53 | 2.8715 |
| $\mathrm{P}_{\mathrm{CAY}}$ | -2.67 | -2.215 | 20.5418 |
| $\mathrm{M}_{\mathrm{CA}}$ | 2.7 | 3.047 | 11.38825 |
| $\mathrm{P}_{\text {EDX }}$ | 13.93 | 13.53 | 2.8715 |
| $\mathrm{P}_{\text {EDY }}$ | -2.67 | -2.215 | 20.5418 |
| $\mathrm{M}_{\text {ED }}$ | 53.3 | 47.34 | 11.18199 |
| $\mathrm{P}_{\text {EFX }}$ | -2.67 | -2.215 | 20.5418 |
| $\mathrm{P}_{\text {EFY }}$ | 13.93 | -13.53 | 2.95639 |
| $\mathrm{M}_{\text {EF }}$ | -53.3 | -47.34 | 12.5898 |
| $\mathrm{P}_{\text {GHX }}$ | -1.78 | -2.215 | 24.4382 |
| $\mathrm{P}_{\text {GHY }}$ | 6.07 | 6.468 | 6.15337 |
| $\mathrm{M}_{\text {GH }}$ | 35.5 | 23.29 | 34.39437 |
| $\mathrm{P}_{\text {HGX }}$ | 1.78 | 2.215 | 19.63883 |
| $\mathrm{P}_{\text {HGY }}$ | -6.07 | -6.468 | 6.55684 |
| $\mathrm{M}_{\text {HG }}$ | 35.5 | 41.4 | 14.25121 |
| $\mathrm{P}_{\text {HIX }}$ | -6.07 | -6.468 | 6.55684 |
| $\mathrm{P}_{\text {HIY }}$ | -1.78 | -2.215 | 24.4382 |
| $\mathrm{M}_{\text {HI }}$ | -35.5 | -41.4 | 16.6197 |
| $\mathrm{P}_{\text {BJX }}$ | 6.07 | 6.468 | 6.15337 |
| $\mathrm{P}_{\text {BJY }}$ | 17.8 | 18.98 | 6.217071 |
| $\mathrm{M}_{\text {BJ }}$ | 78.9 | 80.94 | 2.520385 |
| $\mathrm{P}_{\text {JBX }}$ | 6.07 | -6.468 | 6.55684 |
| $\mathrm{P}_{\text {JBY }}$ | 17.8 | -18.98 | 6.62921 |
| $\mathrm{M}_{\text {JB }}$ | 106.2 | 108.9 | 2.479339 |

All results obtained are compared and the \% difference between the MS excel and the Textbook are within the acceptable range.

Several examples were considered using other softwares like Matlab, Abaqus, Winkler's method and the MS Excel. The results obtained and the percentage differences were calculated and submitted to the department of Civil Engineering in Niger Delta University, Amassoma, Bayelsa State and the results were approved by Dr. Solomon T. Orumu, Professor Adewumi K. Ife and the department for my masters degree dissertation.

## 6. CONCLUSION

From the results shown in the above example, it can be said that the MS Excel spreadsheet develop using the stiffness matrix method yields an approximate result to the Abaqus software results. The developed MS Excel Spreadsheet

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Program can be used to analyze curved beams and for every computer literate that can use the Ms Excel Spreadsheet even if you do not know how to use Abaqus, Ansy, FEM, etc, which are not available on all computers.
Based on the results obtained from the example above, the stiffness matrix method of curved beam analysis gives an approximate result to the exact method. The following recommendations are made:

1. The method is an approximate method
2. An increase in the number of straight lines would yield more accurate results.
3. The longer the length of the curve, more straight lines are required.
4. A more familiar software (MS-Excel Spreadsheet) can be used to solve analyze curved beam elements.

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